1) $A$
2) $D$
3) 

$$
\begin{align*}
& 1 / 2 \mathrm{mv}^{2}=m \mathrm{c} \Delta \theta+\mathrm{mL}  \tag{2}\\
& \mathrm{v}^{2}=2 \mathrm{c} \Delta \theta+2 \mathrm{~L} \\
& \mathrm{v}^{2}=2 \times 126 \times 300+2 \times 21,000  \tag{1}\\
& \mathrm{v}=340 \mathrm{~ms}^{-1} \tag{1}
\end{align*}
$$

[TOTAL 4]
4)
(a) $m c \theta$ (or similar) used.
$c=(2100 \times 240) /(1.50 \times 80)$
$=4200 \mathrm{~J} \mathrm{~kg}^{-1} \mathrm{~K}^{-1}$ (unit required: working must be shown)
(2)
[3]
(b) $\quad \mathrm{mL}$ (or similar) used

$$
\begin{equation*}
L=(2100 \times 800) / 0.75 \tag{1}
\end{equation*}
$$

$=2.24 \times 10^{6} \mathrm{~J} \mathrm{~kg}^{-1} \quad$ (unit required): working must be shown)
(c) appreciation that volume and length are in a power 3 reiation
ratio of volumes of steam and water $=1600$
ratio of mean separations $=(1600)^{1 / 3}=11.7$
5)

Placing a liquid in a vacuum (e.g. a leak from a space vehicle) forces it to evaporate and can lead to rapid cooling.
a. $\mathrm{mc} \Delta \mathrm{T}=0.01 \mathrm{~mL}$ hence $\Delta \mathrm{T}=0.01 \mathrm{~L} / \mathrm{c}=.01 \times 2.26 \times 10^{6} / 4200=5.4^{\circ} \mathrm{C}$ $\nabla$, new temperature (assuming no other losses) is $4.6^{\circ} \mathrm{C} \nabla$
b. All factors lead to rapid evaporation and thus heat loss and sensation of cold owtte $\nabla$
c. Draught enhances evaporation rate. Thus faster cooling owtte $\square$
d. More volatile liquids evaporate even faster $\qquad$
6)
a) Mass $=V \times \rho=8 \times 20 \times 2 \times 1000=3.2 \times 10^{5} \mathrm{~kg}$ $\nabla$
b) $\quad Q=m c \Delta T=3.2 \times 10^{5} \times 4200 \times 1=1.3 \times 10^{9} \mathrm{~J}$
c) $5000 \times 3600 \times 24 \times 200=8.6 \times 10^{10} \mathrm{~J}$ $\nabla$
d) $\quad \Delta T=8.5 \times 10^{10} / 1.3 \times 10^{9}=64 \mathrm{~K}$ マ

No losses to the environment
$\nabla$
e) It would freeze up and block the heat extraction mechanism $\nabla$ just above freezing point $\nabla$, assuming that the water is adequately circulated.
f) $65^{\circ} \mathrm{C}$ allowing for rounding errors: accept $64^{\circ} \mathrm{C}$
g) Plainly impractical as open bodies of water in the UK do not reach this temperature. If they did, they would be dangerous for bathing. However, the idea might be useful as a supplement to other energy sources. Alternatively, a dedicated water-filled heat reservoir in conjunction with a solar capture system may have some practical value. Basic answer $\nabla$; expansion on ideas $\nabla$

Total 10 『
7)
a) $\quad \Delta E=75 \times 4,200$
$=315,000 \mathrm{~J}$ or $\mathrm{J} /{ }^{\circ} \mathrm{C} \quad \checkmark \quad$ a unit needed
b)
$240 / 315,000\left({ }^{\circ} \mathrm{C} /\right.$ second)
$7.6 \times 10^{-4} \quad{ }^{\circ} \mathrm{C} /$ second
Or inverse $\quad 1312$ seconds/ ${ }^{\circ} C \quad$ the units must make the answer clear
c) For $2{ }^{\circ} \mathrm{C} \quad \Delta t=2 / 7.6 \times 10^{-4}=2,600$ seconds ( $=44$ minutes)

Total 5
8)
(a) No heater $\frac{\Delta \mathrm{m}}{\Delta \mathrm{t}}=0.330 \mathrm{~g} \mathrm{~s}^{-1}$

With heater $\quad \frac{\Delta \mathrm{m}}{\Delta \mathrm{t}}=0.350 \mathrm{~g} \mathrm{~s}^{-1}$
Must be a clear indication of which is which and units needed.
(b) Electrical power $=V \times I=3.9 \times 1.2$

$$
\begin{equation*}
=4.68=4.7 \mathrm{~W} \tag{2}
\end{equation*}
$$

(b) $\begin{aligned} \text { Electrical } & =4.68=4.7 \mathrm{~W}\end{aligned}$
(c) $\quad 4.68 \mathrm{~J} / \mathrm{s}$ boils away $0.020 \mathrm{~g} / \mathrm{s}$

So 234 J needed to boil away 1 g
owtte
(d) $234 \mathrm{~J} / \mathrm{g} \mathrm{x} 0.330 \mathrm{~g} / \mathrm{s}$

$$
\begin{equation*}
=77 \mathrm{~W} \tag{2}
\end{equation*}
$$

(e) Mass of liquid nitrogen $=\rho \mathrm{V}$

$$
\begin{aligned}
& =810 \frac{\mathrm{~kg}}{\mathrm{~m}^{3}} \times \frac{25}{1000} \frac{\text { litres }}{\text { litres } \mathrm{m}^{-3}} \\
& =20.3 \mathrm{~kg} \\
\text { Heat Energy required } & =20.3(\mathrm{~kg}) \times 1000(\mathrm{~g} / \mathrm{kg}) \times 234(\mathrm{~J} / \mathrm{g}) \\
& =4.7(5) \times 10^{6} \mathrm{~J} \\
\text { Power input to Dewar } & =\frac{4.75 \times 10^{6}}{100 \times 24 \times 3600} \quad 100 \text { days in seconds } \\
& =0.55 \mathrm{~W}
\end{aligned}
$$

[Q5: 12 marks]
9)

$$
\begin{aligned}
\Delta Q & =m c \Delta T ; m=\rho V \\
\Delta Q & =(10 \times 10 \times 15) \times 10^{-3} \times 4.2 \times 10^{3} \times(100-20) \\
& =5.0 \times 10^{5} \mathrm{~J}
\end{aligned}
$$

b)

Decrease in pressure
c)

New boiling point: $100-(6000 \div 300)=80^{\circ} \mathrm{C}$

$$
\begin{aligned}
\Delta Q & =m c \Delta T=100 \times 10^{-3} \times 4.2 \times 10^{3} \times(80-10) \\
& =3 \times 10^{4} \mathrm{~J}
\end{aligned}
$$

d)

Assuming the stove was working properly at sea level,

$$
\begin{aligned}
\text { time } & =\left(\frac{3 \times 10^{4}}{5 \times 10^{5}} \times 15 \times 60\right) \times 2 \\
& =108 \mathrm{~s}
\end{aligned}
$$

| Question |  |  | Answers | Notes | Total |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | a |  | $\begin{aligned} & \text { weight of cylinder }=A h g \rho \\ & \text { pressure }=\frac{F}{A}=\frac{A h g \rho}{A} \end{aligned}$ |  | 2 |
| 10 | b | i | use of $P V=n R T$ and $V=$ Area $\times(0.190)$ seen $\checkmark$ substitution of $\mathrm{P}=p_{\mathrm{o}}+p_{\mathrm{m}}$ 《re-arrangement to give answer» $\checkmark$ |  | 2 |
| 10 | b | ii | recognition that $\frac{\mathrm{nRT}}{\mathrm{A}}$ is constant $O R 190 p_{\mathrm{o}}+190 p_{\mathrm{m}}=208 p_{0}-208 p_{\mathrm{m}}$ OR $p_{0}=\frac{398}{18} p_{\mathrm{m}} \checkmark$ pressure due to mercury $p_{\mathrm{m}}=0.035 \times 1.36 \times 10^{4} \times 9.81\left(=4.67 \times 10^{3} \mathrm{~Pa}\right) \checkmark$ $1.03 \times 10^{5} \checkmark$ <br> $\mathrm{Pa} O \boldsymbol{O} \mathrm{Nm}^{-2} \mathbf{O R} \mathrm{kgm}^{-1} \mathrm{~s}^{-2} \checkmark$ | Award MP4 for any correct unit of pressure (eg "mm of mercury / Hg"). | 4 |
| 10 | b | iii | same number of particles to collide with a larger surface area $\operatorname{OR}$ greater volume with constant rms speed decreases collision frequency $\checkmark$ |  | 1 |

