

Marking Scheme

Question	Marking details	Marks available				Maths	Prac
		AO1	AO2	AO3	Total		
2 (a)	Use of Snell's law (1), e.g. $\sin 18.4^\circ = 1.65 \sin \theta_2$ Manipulation or Answer = 11.0° (1) accept $\sin^{-1}\left(\frac{\sin 18.4^\circ}{1.65}\right)$ but not just 10°	1	1		2	1	
(b)	$\phi = 90 - \theta$ (79 or 80) (1) $n_2 \sin \theta_2 = n_3 \sin 90$ applied (1) or $n_2 \sin 79 = n_3 \sin \theta$ Answer = 73.2° (1) or no solution for θ Conclusion = Yes since ϕ greater than critical (1) [allow ecf on a calculated value of critical angle] or Yes refraction is impossible			4	4	3	
	Question 2 total	1	1	4	6	4	0

Question	Marking details	Marks available				Maths	Prac
		AO1	AO2	AO3	Total		
3 (a)	Refraction is a change in direction of the travel of waves (1) Waves travel more slowly in glass than in air (1) Therefore AB is greater than CD (1)	1 1	1		3		
(b)	Measuring lengths AB = 2.9 cm and CD = 1.8 cm within 0.1 cm (1) Speed = $\frac{BD}{t}$ and $\frac{AC}{t}$ (can be implied) (ecf) (1) Speed = 1.9 [or 1.86] $\times 10^8$ [m s ⁻¹] (1)	1	1 1		3	2	
	Question 3 total	3	3	0	6	2	0

Question	Marking details	Marks available				Maths	Prac
		AO1	AO2	AO3	Total		
7 (a) (i)	$1.00 \sin \theta_{air} = 1.60 \sin 30^\circ$ or equivalent or by implication (1) $\theta_{air} = 53^\circ$ (1) Beam bends sharply to the left at the surface (1)	1	1 1		3	2	
(ii)	$\theta = \theta_c$ or by implication (1) $\sin \theta = \frac{1}{1.60}$ [=0.625] or equivalent (eg $\theta_c = 39^\circ$) (1) $x = 62.5 / 63$ mm (1)	1 1	1		3	2	
(b)	Marking points A1. Light [travelling at small angles to axis] hitting core/cladding boundary is totally internally reflected A2. [So] transmitted along fibre without loss B3. Light paths at different angles [to axis] are of different lengths [for given length of fibre] B4. [So] take [slightly] different times and [so] [each] pulse spread out [over time] on arrival at far end C5. Pulses may overlap (if in rapid sequence) C6. Spreading [accept mm dispersion] increases with length of fibre, [so] overlap more likely if fibre longer 5-6 marks Expect at least 4 points made from all of sections A, B and C There is a sustained line of reasoning which is coherent, relevant, substantiated and logically structured. 3-4 marks Expect at least 3 points made from at least two sections from A, B or C There is a line of reasoning which is partially coherent, largely relevant, supported by some evidence and with some structure. 1-2 marks Any 2 points made There is a basic line of reasoning which is not coherent, largely irrelevant, supported by limited evidence and with very little structure. 0 marks No attempt made or no response worthy of credit.	6			6		
	Question 7 total	9	3	0	12	4	0

4.

Question			Marking details	Marks available					
				AO1	AO2	AO3	Total	Maths	Prac
7.	(a)	(i)	$v_{\text{plastic}} = \frac{AC}{BD} \times c \text{ or equivalent or by implication (1)}$ $BD = 44 \text{ or } 45 \text{ or } 46 \text{ [mm]; } AC = 31 \text{ or } 32 \text{ or } 33 \text{ [mm] (1)}$ $v_{\text{plastic}} = (2.1 \pm 0.1) \times 10^8 \text{ [m s}^{-1}\text{] (1)}$		3		3	3	
		(ii)	$n = 1.4 [\pm 0.1] \text{ ecf}$		1		1	1	
	(b)	(i)	A correct relevant time calculation e.g. for 120 m, 608 ns or for 120.9 m, 613 ns or by implication (1) Extra time by zig-zag route = 5 ns [4.6 ns] (1) Therefore overlap will occur, [as 4.6 ns > 4.0 ns] no ecf (1) [Allow 1 mark if n (refractive index) omitted leading to 3.0 ns delay and hence no overlap] Alternative: Extra distance for 4.0 ns extra time $\frac{3.00 \times 10^8 \times 4.0 \times 10^{-9}}{1.52}$ (1) = 0.79 [m] (1) Therefore overlap will occur [as 0.79 < 0.90 m] (1) [Allow 1 mark if n (refractive index) omitted leading to 1.2 m delay and hence no overlap]			3	3	2	
		(ii)	$n_{\text{clad}} [\sin 90^\circ] = 1.520 \sin 83^\circ \text{ or equivalent (1)}$ $n_{\text{clad}} [\sin 90^\circ] = 1.51 \text{ (1)}$		2		2	2	
			Question 7 total	0	6	3	9	8	0

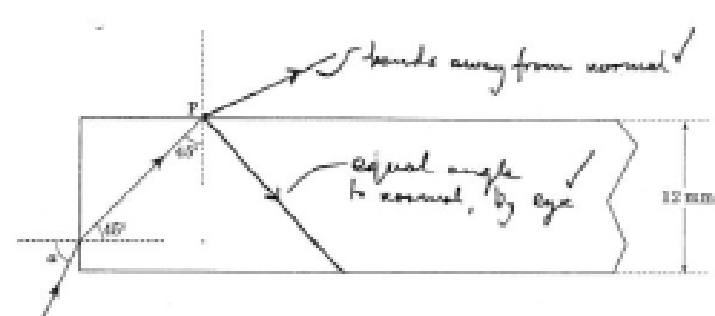
5.

Question			Marking details	Marks available					
				AO1	AO2	AO3	Total	Maths	Prac
6	(a)	(i)	$\text{Rearranging } \sin c = \frac{1.47 \sin 90}{1.52} \text{ (1)}$ $\text{Critical angle} = 75.3^\circ \text{ (1)}$		2		2	2	
		(ii)	$\text{Substitution into Snell's law i.e. } \sin 15^\circ = 1.52 \sin \theta_r \text{ (1)}$ $\text{Refracted angle} = 9.8^\circ \text{ (1)}$ $A = 80.2^\circ (90 - \theta_r) \text{ (ecf on } \theta_r) \text{ (1)}$	1	1 1		3	2	
		(iii)	Angle A is greater than critical angle (ecf on A and critical angle) (1) So total internal reflection and light will travel down the fibre OR technician not correct (1)			2	2		
	(b)		$\text{Substituting values in } \text{speed} = \frac{\text{distance}}{\text{time}} \text{ (1)}$ $\text{Speed of light in fibre} = \frac{c}{1.52} \text{ (1)}$ $\text{Time} = 7.6 \times 10^{-5} \text{ s (1)}$	1	1 1		3	3	
	(c)	(i)	Monomode – parallel to axis/straight – Multimode zig zag paths	1			1		
		(ii)	No spreading of pulses OR only one path for data (1) Each pulse arrives at same time OR No overlapping of pulses (1) Allows faster rate of data transfer (1)	3			3		
			Question 6 total	6	6	2	14	7	0

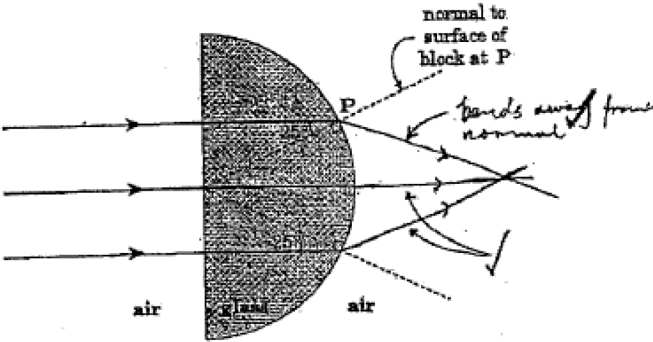
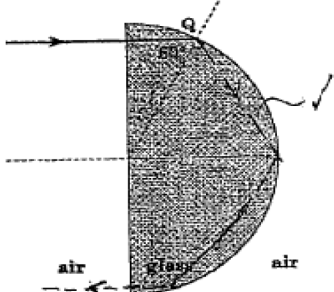
Question		Marking details	Marks available				Maths	Prac
			AO1	AO2	AO3	Total		
8	(a)	[Constant] velocity horizontal (1) Accelerating / force downwards [b.o.d. motion under gravity] (1) Projectile motion → 1 mark		2		2		
	(b)	$\phi = \sin^{-1}\left(\frac{1.55}{1.58}\right)$ (1) 78.82°, 78.8° or 79° etc. seen (not just 80) (1) 1.38 [rad] → 1st mark	1	1		2	2	
	(c)	Maximum angle for propagation with TIR (1) Rotational symmetry (about central axis) (1)		2		2		
	(d)	$\theta_2 = 90 - 80 = 10$ degree or similar (11.2 degree etc.) (1) $n_1 \sin \theta_1 = n_2 \sin \theta_2$ used (1) Rearrangement $\theta_1 = \sin^{-1}\left(\frac{n_2 \sin \theta_2}{n_1}\right)$ (1) Answer = 17.9° or 15.9° if 10° used (1)	1	1 1		4	3	
	(e)	Dispersion increases with length of fibre (1) [Maximum] bit rate and distance proportional [however stated, eg. Accept distance × 10 → bit-rate down by factor of 10] (1) Conclusion consistent with argument (1)			3	3		
	(f)	20 × 0.8 dB or 16 dB seen (1) Correct comparison with table e.g. 15 dB too much (0.03) (1) Correct conclusion: no, signal drops too much / distance too large (1) [NB Either distance for 6% = 15.3 km or 20 km → 2.5 % gives the first two marks].			3	3	2	
	(g)	Wavelength is decreased by factor n or $v=c/n$ (1) Wavelength is 820 nm (1) So thickness of around 8.2 μm is required (1) 13 μm student is wrong (1) [Allow Aled correct because 1.3 μm × 10 = 13 μm for 1 mark]			4	4	2	
		Question 8 total	2	8	10	20	9	0

7.	(a)	$n_{\text{clad}} \sin 90^\circ = 1.540 \sin 77^\circ$ or $n_{\text{clad}} = 1.540 \sin 77^\circ$ [or by impl.] (1) $n_{\text{clad}} = 1.50[1]$ [accept 1.5] (1)
	(b)	(i) $\text{speed} = \frac{3.00 \times 10^8}{1.54}$ (1) $\text{time} = \frac{\text{distance}}{\text{speed}}$ (1) [transposed at any stage] $= 1.027 \times 10^{-5} \text{ s}$ (1) [omission of 1.54 loses just 1 mark] (ii) I. $AB = \frac{AC}{\sin 77^\circ}$ or $AB = \frac{AC}{\cos 13^\circ}$ or equiv. (1) II. Zigzag time $= 1.027 \times 10^{-5} \times 1.026 \text{ s}$ (1) [or Extra time $= 1.027 \times 10^{-5} \times 0.026$ or by impl.] Extra time $= 2.7 \times 10^{-7} \text{ s}$ [e.c.f. on speed] (1) (iii) Bit of data arrives spread out over a period of time [accept: data smeared or multimode dispersion] (1). Data bits could overlap on arrival / can't distinguish (1)

8.	2	(a)	(i) $v_{\text{air}} > v_{\text{glass}}$ (1), $f_{\text{air}} = f_{\text{glass}}$ and $\lambda_{\text{air}} > \lambda_{\text{glass}}$ (1) (ii) Cycles [or oscillation] can't appear or disappear [at boundary] or equiv. / frequency determined by the source [not just f is constant]	2 1
		(b)	(i) $[1.00] \sin 40^\circ = 1.52 \sin \phi$ [where ϕ = angle of refraction] (1) $\phi = 25^\circ$ (1); $\theta = 90^\circ - 25^\circ$ (1) = $[65^\circ]$ (ii) $\sin c = \frac{1}{1.52}$ [or equiv] or: $c = 41^\circ$ (1) $\sin^{-1}(1.52 \sin 65^\circ)$ gives "error" $65^\circ > 41^\circ$ or remark (1) [free standing] (1), so refraction not possible (1)	3 2
		(iii)	I. Diagram: Reasonable path drawn [no gross departure from law of reflection] with emergent ray in correct quadrant (1) II. 2 sensible parallel paths inside block labelled (1) Emergent ray labelled as parallel to incident ray. (1)	1 2
		(c)	Any $2 \times (1)$ from: - minimises <u>multimode</u> dispersion [or equiv](✓) - cuts down range of path lengths (✓) - less pulse broadening or less likelihood of overlapping or more rapid data [allow: smearing and jumbling] sequence possible (✓) [not interfere or distorted]	2 [13]

(a)		Award 3 x (1) of: • Refraction is change in direction of travel as waves change medium / air to glass (or equivalent). • AB, CD are wavefronts (or peaks or crests). • AB goes to CD. • Waves travel more <u>slowly</u> in 2 than in 1. • Hence $BD < AC$ Accept wavelength less in medium 2. • Direction of travel of waves is normal to wavefronts.	[3]
(b)	(i)	$[1.00] \sin \alpha = 1.33 \sin 45^\circ$ (1) or equivalent or by implication	[2]
	(ii)	I	[2]
		 No need for arrow heads. No penalty if reflected ray doesn't reach the bottom of the fibre.	[2]
	(ii)	II 6 reflections needed [including that at P] (1) Light travels 12 mm parallel to rod axis between successive reflections. (1) or by implication Light has to travel 60 [mm] beyond P (1) Accept 72 [mm] Award 2 marks for $17 \text{ mm} \times 5 = 85 \text{ [mm]}$ Award 1 mark for $17 \text{ mm} \times 6 = 102 \text{ [mm]}$	[3]
(c)	(i)	$c = 49^\circ$ (1) $50^\circ > 49^\circ$ or $50^\circ > c$ AND so refraction not possible / TIR / no power loss (1)	[2]
	(ii)	Total internal reflection	[1]

10. (a)	(i) $v_{\text{air}} > v_{\text{glass}}$ (1), $f_{\text{air}} = f_{\text{glass}}$ and $\lambda_{\text{air}} > \lambda_{\text{glass}}$ (1)	2
	(ii) Cycles [or oscillation] can't appear or disappear [at boundary] or equiv. / frequency determined by the source [not just f is constant]	1
(b)	(i) $[1.00] \sin 40^\circ = 1.52 \sin \phi$ [where ϕ = angle of refraction] (1) $\phi = 25^\circ$ (1); $\theta = 90^\circ - 25^\circ$ (1) = $[65^\circ]$	3
	(ii) $\sin c = \frac{1}{1.52}$ [or equiv] or: $c = 41^\circ$ (1) $65^\circ > 41^\circ$ or remark (1)[free standing] $\sin^{-1}(1.52 \sin 65^\circ)$ gives "error" (1), so refraction not possible (1)	2
	(iii) I. Diagram: Reasonable path drawn [no gross departure from law of reflection] with emergent ray in correct quadrant (1)	1
	II. 2 sensible parallel paths inside block labelled (1) Emergent ray labelled as parallel to incident ray. (1)	2
(c)	Any 2 $\times$ (1) from: - minimises <u>multimode</u> dispersion [or equiv](✓) - cuts down range of path lengths (✓) - less pulse broadening or less likelihood of overlapping or more rapid data [allow: smearing and jumbling] sequence possible (✓) [not interfere or distorted]	2 [13]

Question			Marking details	Marks Available
	(a)	(i)	(I)  (II) $1.58 \sin 25^\circ = [1.00] \sin a$ (1) or equivalent or by implication $a = 42^\circ$ (1)	[2]
		(ii)	(I) Either $c = 39^\circ$ (1) $60^\circ > 39^\circ$ or equivalent (1) OR $1.58 \sin 60^\circ$ gives error (1) So refraction not possible or TIR [needs attempt to justify] (1) (II) TIR at Q and at least one more instance of TIR with subsequent ecf (1) As drawn with reflected ray at Q going off East of South, eventually emerging through diameter face, with at least one more TIR event.(1) 	[2]
	(b)	(i)	Thinner	[1]
		(ii)	Monomode: parallel to axis (accept straight) Multimode: zig-zag paths as well (1) or some paths involve reflections	[1]
		(iii)	Only one route for data (1) [no zig-zag routes] Each pulse [data element etc] arrives [at other end of fibre] at same time (1) No overlapping of pulses (1) [even over long distances]	[3]
			Question 3 Total	[13]

12.	(a)	(i)	medium 1: $2.0 \times 10^8 \text{ [m s}^{-1}\text{]}$ and medium 2: $2.5 \times 10^8 \text{ [m s}^{-1}\text{]}$	1
		(ii)	Correct use of $\sin 30^\circ$ seen clearly (1) Rest of argument, including use of $t = \frac{d}{v}$ [ecf on v and on value of $\sin 30^\circ$, if failure to reach the stated time is noted]. (1)	2
		(iii)	$BD = 2.5 \times 10^8 \text{ ecf} \times 2.5 \times 10^{-11} \text{ [m]} [= 6.25 \text{ mm}]$ or by implication (1) $\theta_2 = 38.7^\circ$ (or 39°) ecf on $v = 2.5 \times 10^8 \text{ [m s}^{-1}\text{]}$ (1)	2
		(iv)	$1.50 \sin 30^\circ = 1.20 \sin \theta_2$ (1) Therefore $\theta_2 = 38.7^\circ$ (or 39°) no ecf (1)	2
	(b)	(i)	Use of $v = 2.0 \times 10^8 \text{ [m s}^{-1}\text{]}$ (1) $t = \frac{1600}{2.0 \times 10^8} \text{ [s]}$ ecf on v (1)	2
		(ii)	Critical angle = 76° or by implication (1) $n_{\text{clad}} [\times \sin 90^\circ] = 1.500 \sin 76^\circ$ ecf on 76° or by implication (1) $n_{\text{clad}} = 1.455$ or 1.46 do not accept 1.45 no ecf (1)	3
		(iii)	$\frac{AC}{AB} = \cos 14^\circ$ or equivalent or by implication (1) $\Delta t = 0.24 \mu\text{s}$ ecf on v (1)	2

(a)	(i)	Smooth curve drawn through all the points	1														
	(ii)	46° [or as appropriate from drawn line]	1														
	(iii)	Reflected ray drawn with angle of reflection equal to θ by eye.	1														
	(iv)	Any of:															
		<table> <tr> <td>$\frac{\sin 14^\circ}{\sin 10^\circ} \checkmark$</td> <td>$\frac{\sin 28.5^\circ}{\sin 20^\circ}$</td> <td>$\frac{\sin 44^\circ}{\sin 30^\circ}$</td> <td>$\frac{\sin 64^\circ}{\sin 40^\circ}$</td> <td>$\frac{\sin 82^\circ}{\sin 45^\circ}$</td> </tr> <tr> <td>1.39 [±0.05] ✓</td> <td>1.40 [±0.05]</td> <td>1.40 [±0.05]</td> <td>1.40 [±0.05]</td> <td>1.40 [±0.05]</td> </tr> <tr> <td>or by implication</td> <td></td> <td></td> <td></td> <td></td> </tr> </table>	$\frac{\sin 14^\circ}{\sin 10^\circ} \checkmark$	$\frac{\sin 28.5^\circ}{\sin 20^\circ}$	$\frac{\sin 44^\circ}{\sin 30^\circ}$	$\frac{\sin 64^\circ}{\sin 40^\circ}$	$\frac{\sin 82^\circ}{\sin 45^\circ}$	1.39 [±0.05] ✓	1.40 [±0.05]	1.40 [±0.05]	1.40 [±0.05]	1.40 [±0.05]	or by implication				
$\frac{\sin 14^\circ}{\sin 10^\circ} \checkmark$	$\frac{\sin 28.5^\circ}{\sin 20^\circ}$	$\frac{\sin 44^\circ}{\sin 30^\circ}$	$\frac{\sin 64^\circ}{\sin 40^\circ}$	$\frac{\sin 82^\circ}{\sin 45^\circ}$													
1.39 [±0.05] ✓	1.40 [±0.05]	1.40 [±0.05]	1.40 [±0.05]	1.40 [±0.05]													
or by implication																	
(v)	I.	Any 2 × (1) from															
		- Straight ✓ - Through the origin ✓ - Gradient > 1 ✓	2														
	II.	[n is the] gradient	1														
(b)	(i)	1.530 sin c = 1.520 [sin 90°] (1) [or by impl.]															
		c = 83° (1)	2														
	(ii)	$\theta = 7^\circ$ [accept 6.5°] e.c.f. from (b)(i)	1														
	(iii)	Smaller <u>differences</u> in distances travelled or times taken [by light travelling different paths] (1), so less blurring / smearing / overlap of data / pulses (1) [or data can be transmitted at a greater rate]															
		Less multimode dispersion only award 2 nd mark	2														

Question			Marking details	Marks Available
4	(a)	(i)	$\sin \theta = 1.331 \sin 40.36^\circ$ or by implication (1) 60° (1) Accept 59.5°	2
		(ii)	<i>Not</i> total + attempt at justification even if not worth next mark (1) For the 2nd mark either: Light got in at P or gets out at R, so can get out at Q [as angles in water the same] or $1.331 \sin 40.36$ reshown to be < 1 or $C = 49^\circ$	2
		(iii)	$v_{\text{violet}} < v_{\text{red}}$ + attempt at justification even if not worth next mark e.g. violet bends more (1) For the 2nd mark either: Violet must have larger n therefore smaller v or bending caused by light travelling more slowly in water than in air, so violet must travel most slowly.	2
	(b)	(i)	Speed in glass = $\frac{360}{1.75 \times 10^{-6}}$ [= $2.06 \times 10^8 \text{ m s}^{-1}$] or by implication (1) $n = 1.46$ (1) must be to 3 sig figs	2
		(ii)	$C = 75^\circ$ or by implication (1) $1.46 \sin 75^\circ = n_{\text{clad}} [\sin 90^\circ]$ [Accept 1.5 for 1.46] or by implic (1) $n_{\text{clad}} = 1.41$ [1.45 if n_{core} taken as 1.50] (1) Award 1 mark only for: $1.46 \sin 15^\circ = n_{\text{clad}} [\sin 90^\circ]$	3
		(iii)	Larger angles give longer propagation times. [Accept longer dists.](1) So each pulse spread out over time on arrival or each pulse is less spread out if the angles are restricted (1) So pulses might overlap (Accept pulses muddled) or overlap/muddling of pulses less likely if angles restricted. (1) Award 1 mark only for less multimode dispersion	3
			Question 4 Total	[14]